

Virtual Simulation Lab: Comparing VIRGO with an Experimental Measurement

In this post, we compare a VIRGO simulation of the diffusion coefficient of a hemicylinder with an experimental measurement from the 2D boundary plane goniometer.

In Figure 1, we show a schematic illustration of the 2D VIRGO goniometer. In order to create high-resolution polar responses, we are using a larger number of virtual microphones than are used experimentally.

2D:

- Number of microphones: 180
- θ spacing: 1°

In Figure 2, we compare the normal incidence normalized diffusion coefficient (top left) between the VIRGO simulation and the experimental measurement, according to ISO 17497-2. The excellent agreement is a testament to the validity of the boundary element simulation. In Figure 2 (top right), we compare the random incidence normalized diffusion coefficients, which also show an excellent agreement. In Figure 2 (bottom), we compare the normal incidence polar responses at three frequencies. Since VIRGO uses 180 microphones versus 37 for the experimental measurement, the simulation shows a higher resolution at 4,000 Hz.

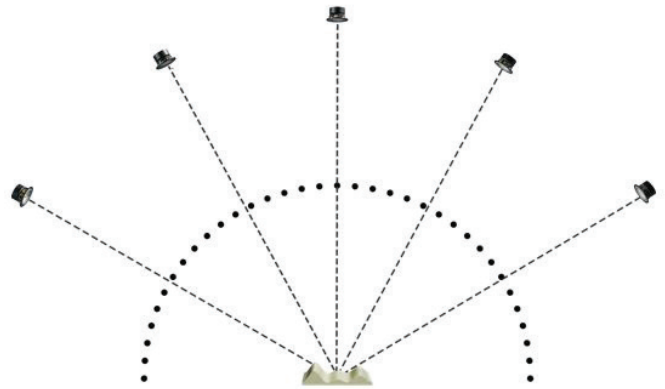


Figure 1. 2D Virtual Goniometer

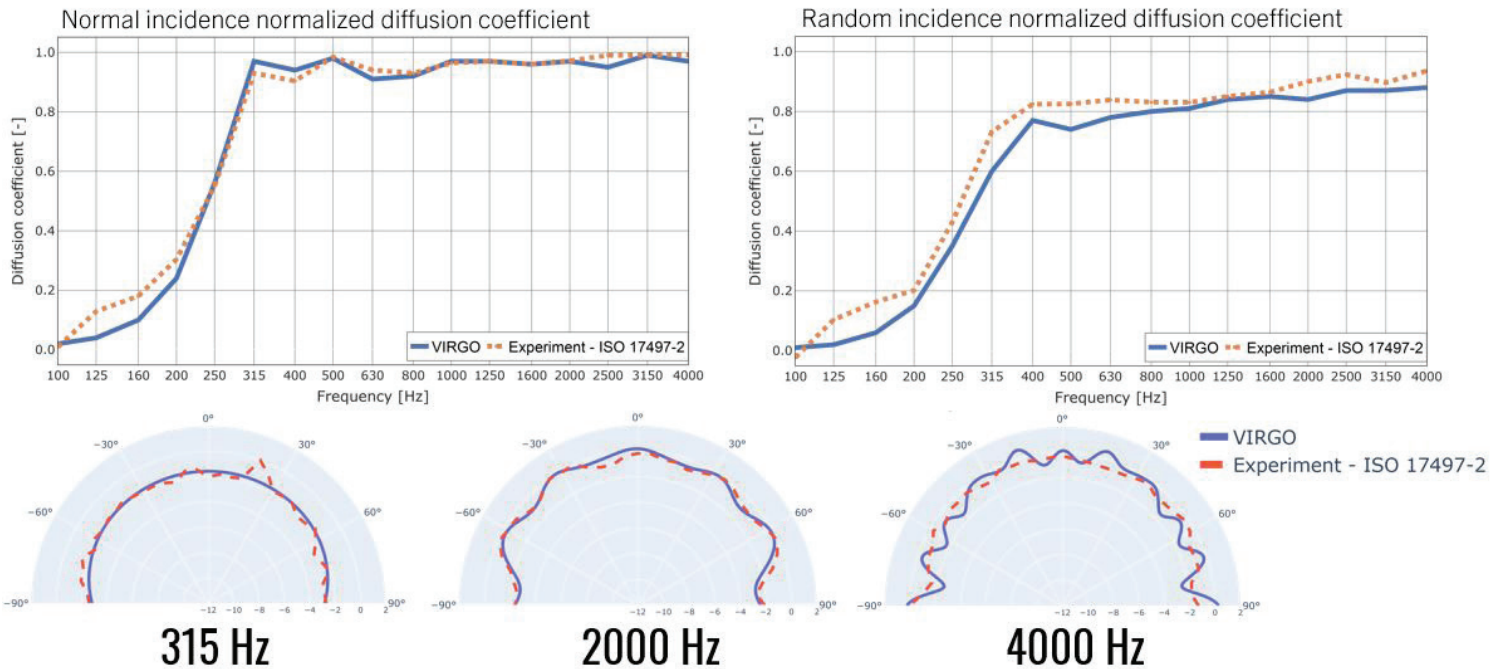


Figure 2. Top: Hemicylinder simulation versus experimental measurement for normal incidence (left) and random incidence (right); Bottom: Polar response comparison for normal incidence at three frequencies.

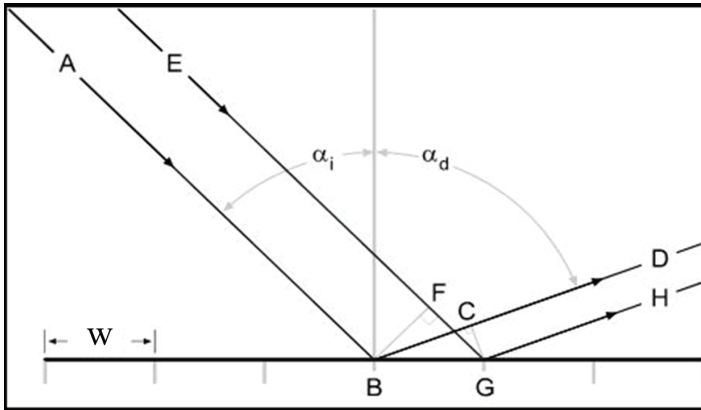


Figure 3. Constructive interference schematic.

The results in Figure 2 are for 1 hemicylinder. When a periodic array is measured the constructive interference generates grating lobes. Figure 3 shows the constructive interference schematic. For a given wavelength, λ , angle of incidence, α_i , and sample width, w , when $BC-FG=m\lambda$, i.e., an integral number of wavelengths, constructive interference occurs in m orders until $\sin\alpha_d$ exceeds 1. The constructive interference equation relating those variables is shown in Figure 3.

$$\sin \alpha_d = \frac{m\lambda}{w} - \sin \alpha_i$$

Figure 4. Constructive interference equation.

In Figure 5, we illustrate the normal incidence polar response at 2 kHz, for a linear, periodic array of (4) 120 mm diameter hemicylinders. For normal incidence α_i is zero. It can be seen that the 7 diffraction orders, $m=0 \pm 1, \pm 2, \pm 3$, agree with the theoretical prediction.

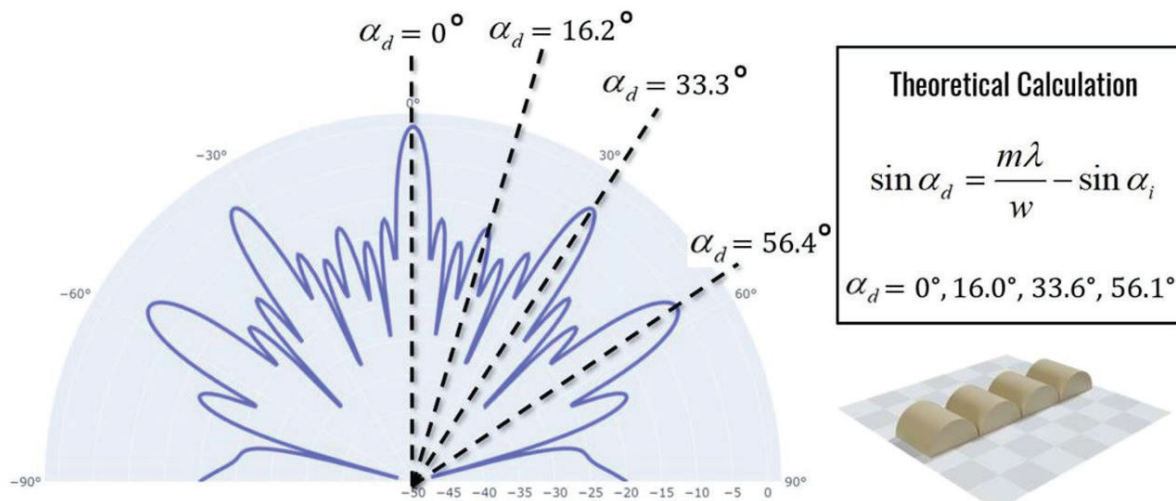


Figure 5. The position for 4 of the 7 diffraction grating lobes, $m=0, m=0 \pm 1, \pm 2, \pm 3$, are indicated to agree with the theoretical calculation

In the next post, we will simulate the scattering from a single hemisphere and a periodic linear and two-dimensional array of hemispheres.



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